

1. (30) In an attempt to reduce the overall pressure drop in a 20.0 m long, 1.00 cm diameter cooling water line, a 16.0 m long segment in the middle of the line is replaced with a 2.00 cm diameter tube. Estimate and compare the pressure drops in these two configurations. The volumetric flow rate is  $2.00 \times 10^{-4} \text{ m}^3/\text{s}$  (which is equivalent to 12.0 liters/min). The density of the water is  $1,002 \text{ kg/m}^3$  and viscosity is  $1.00 \times 10^{-3} \text{ kg/(m}\cdot\text{s)}$  (which is equal to 1.00 cp). Assume smooth surfaces, fully developed flow and an energy correction factor,  $\alpha$ , of 1.00.

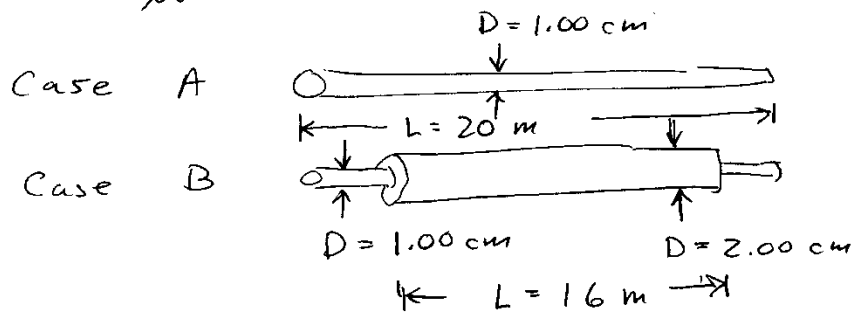
1. Common values (given)

$$\dot{V} = 2.00 \times 10^{-4} \text{ m}^3/\text{s}$$

Assume  $\alpha = 1$

$$\rho = 1,002 \text{ kg/m}^3$$

$$\mu = 1.00 \times 10^{-3} \text{ kg/m}\cdot\text{s}$$



Values in segments

$D \text{ (m)}$	0.01	0.02
$A = \frac{\pi D^2}{4} \text{ (m}^2\text{)}$	$7.85 \times 10^{-5}$	$3.14 \times 10^{-4}$
$V = \dot{V}/A \text{ (m/s)}$	2.55	0.637
$N_{Re} = \frac{\rho V D}{\mu} \text{ (none)}$	25,500	12,800
$f \text{ (from chart)}$	0.026	0.028

"Minor Losses"

$$\text{Expansion } K_{L,e} = \alpha \left(1 - \frac{d^2}{D^2}\right)^2 = \left(\frac{3}{4}\right)^2 = 0.562$$

$$\text{Contraction } K_{L,c} = 0.400 \text{ (at } \frac{d^2}{D^2} \text{ of } 0.25)$$

$$\Delta P_{\text{Pipes}} = f \frac{L}{D} \frac{\rho V^2}{2} \quad 4 \text{ pts}$$

$$\Delta P_L = K_L \frac{\rho V^2}{2} \quad 4 \text{ pts}$$

$\Delta P_L$  for the two cases:

Case 1:  $D = 1.00 \text{ cm}$ ,  $L = 20 \text{ m}$

$$\Delta P_I = 1.69 \times 10^5 \text{ Pa} = \underline{\underline{169 \text{ kPa}}} \quad \begin{array}{l} 10 \text{ pts} \\ -6 \text{ pts if not} \\ \text{determined.} \end{array}$$

Case 2:  $D = 2.00 \text{ cm}$ ,  $L = 16 \text{ m}$  +

$D = 1.00 \text{ cm}$ ,  $L = 4 \text{ m}$  +

sudden Expansion +  
sudden contraction

$$\begin{aligned} \Delta P &= 4.55 \times 10^3 + 3.39 \times 10^4 + 1.83 \times 10^3 + 1.30 \times 10^3 \\ &= 4.16 \times 10^4 \text{ Pa} = \underline{\underline{41.6 \text{ kPa}}} \quad 12 \text{ pts} \end{aligned}$$

So, the pressure drop is less in case 2.

Most wrong - 25

Correct  $K_L$ 's → minor loss  $\Delta P_L$  only - 20

w/ Some correct pipe drops - 10

2. (35) International rules state that ping-pong (table tennis) balls shall weigh 2.7 grams and be 40 millimeters in diameter. What is the terminal velocity of a ping-pong ball at sea level where  $\mu_{\text{air}} = 1.82 \times 10^{-5} \text{ kg/(m}\cdot\text{s)}$ ,  $\rho_{\text{air}} = 1.20 \text{ kg/m}^3$  and  $g = 9.81 \text{ m/s}^2$ ? Neglect buoyancy (I assume it's accounted for in the specified weight of the ball). Without doing any calculations, would a solid depleted uranium ( $\rho = 19.1 \text{ g/cm}^3$ ) ball of the same diameter have a higher or lower terminal velocity under the same conditions?

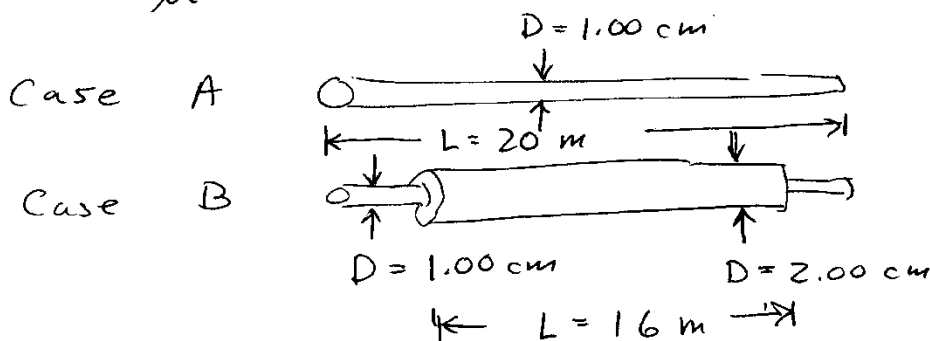
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Assume  $\alpha = 1$



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## Iteration

Guess $v$ (m/s)	$N_{Re}$	$C_D$	$F_D$
1	2630	0.4	$3.01 \times 10^{-4}$
10	26,300	0.4	$3.01 \times 10^{-2}$
9.0	23,700	0.4	$2.44 \times 10^{-2}$

At this point, I know  $9.0 < v < 10$  m/s

In general, I could keep guessing until I found the answer. However, in this case  $C_D$  is not changing,

so just solve  $F_g = \frac{A \rho}{2} C_D v^2$

for  $v$  to get:

$$v = 9.37 \text{ m/s}$$

Depleted uranium would have a higher terminal velocity because the same drag equations would apply but  $F_g$  would be much greater.

For depleted uranium, I get  $v = 332$  m/s

$C_D$  off by  $10 \times -2$

Not showing calc. of  $N_{Re} \Rightarrow C_D -8$

Using Stokes Law - not checking result -20

3. (35) Cross out terms on the given differential balance equations and provide boundary and initial conditions as needed to solve for the steady state velocity distribution in the fully developed flow of an incompressible fluid in a square duct with dimensions  $2W$  wide by  $2H$  high. Align the direction of flow with the  $z$ -axis of your coordinate system. Some credit will be given for choosing the best origin for your coordinate system.

Continuity –

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = 0$$

**Rectangular (Cartesian) Coordinates –**

**x direction**

$$\rho \left( \frac{\partial u_x}{\partial t} + v_x \frac{\partial u_x}{\partial x} + v_y \frac{\partial u_x}{\partial y} + v_z \frac{\partial u_x}{\partial z} \right) = -\frac{\partial p}{\partial x} + \mu \left[ \frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} + \frac{\partial^2 u_x}{\partial z^2} \right] + \rho g_x$$

**y direction**

$$\rho \left( \frac{\partial u_y}{\partial t} + v_x \frac{\partial u_y}{\partial x} + v_y \frac{\partial u_y}{\partial y} + v_z \frac{\partial u_y}{\partial z} \right) = -\frac{\partial p}{\partial y} + \mu \left[ \frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} + \frac{\partial^2 u_y}{\partial z^2} \right] + \rho g_y$$

**z direction**

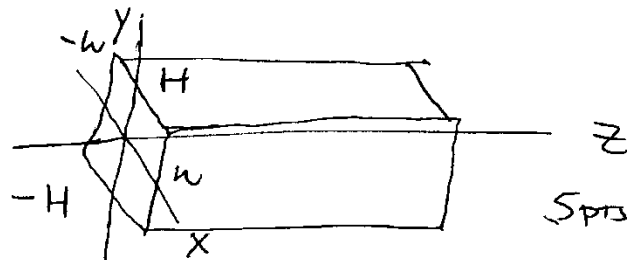
$$\rho \left( \frac{\partial u_z}{\partial t} + v_x \frac{\partial u_z}{\partial x} + v_y \frac{\partial u_z}{\partial y} + v_z \frac{\partial u_z}{\partial z} \right) = -\frac{\partial p}{\partial z} + \mu \left[ \frac{\partial^2 u_z}{\partial x^2} + \frac{\partial^2 u_z}{\partial y^2} + \frac{\partial^2 u_z}{\partial z^2} \right] + \rho g_z$$

Continued on following page...

3. Apply continuity and Navier-Stokes equations.

I.C.'s not required for steady-state problems. 5 pts

Coordinate system



B.C.'s

No slip

$$\begin{cases} u_z = u_x = u_y = 0 & @ \quad x = W \rightarrow -W \\ u_z = u_x = u_y = 0 & @ \quad y = H \rightarrow -H \end{cases}$$

5 pts

sym.

$$\left. \begin{cases} \frac{\partial u_z}{\partial x} = 0 @ x = 0 \\ \frac{\partial u_z}{\partial y} = 0 @ y = 0 \\ u_x = 0 @ x = 0 \\ u_y = 0 @ y = 0 \end{cases} \right\} 5 \text{ pt}$$

## Elimination of terms

- 1) Fully developed implies no changes in the  $z$ -direction 5pts
- 2) Steady state implies no changes with time 5pts
- 3) Neglect pressure changes
- 4) Neglect gravity

Note if continuity is left in, not many other terms can be eliminated. If it is used to claim  $u_y + u_x = 0$  everywhere, terms containing these can be eliminated. However, you can't use both and must explicitly state continuity was used.

Need to comment regarding inclusion of continuity (2pts)

Incompressible implies  $p$  is constant so used incompressible version of continuity.